



# **Wetting Behaviour of Liquid Al-Cu Alloys on Oriented Sapphire Surfaces**

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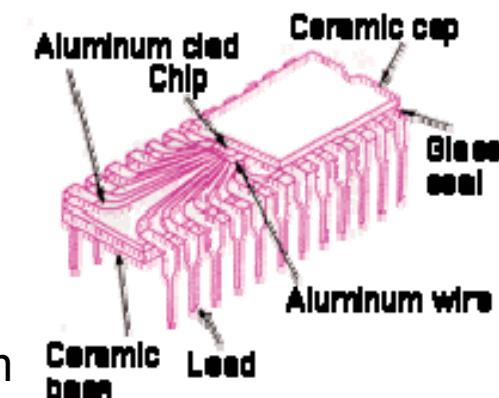
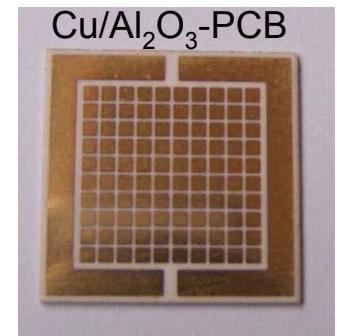


Deutsches Zentrum  
für Luft- und Raumfahrt e.V.  
in der Helmholtz-Gemeinschaft



## Motivation

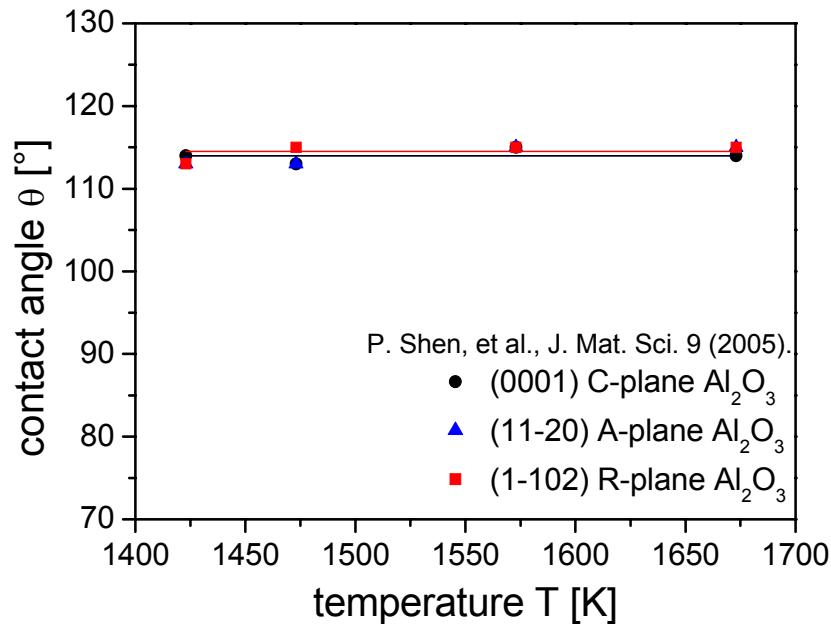
- ↗ Adhesion at M/MO-interface important for technical applications:
  - ↗ Composite materials, Microelectronics
  - ↗ Miniaturisation: System dimensions reach the order of crystallite size
- ↗  $\alpha\text{-Al}_2\text{O}_3$  commonly used oxide crystal
  - ↗ Different kinds of  $\text{Al}_2\text{O}_3$ - surfaces (anisotropy)
  - ↗ Some experiments with pure metals show anisotropy in wetting
- ↗ Al-Cu/ $\text{Al}_2\text{O}_3$  composites with promising properties
  - ↗ Al-Cu basis for solder materials
  - ↗ Anisotropic or isotropic wetting in the system



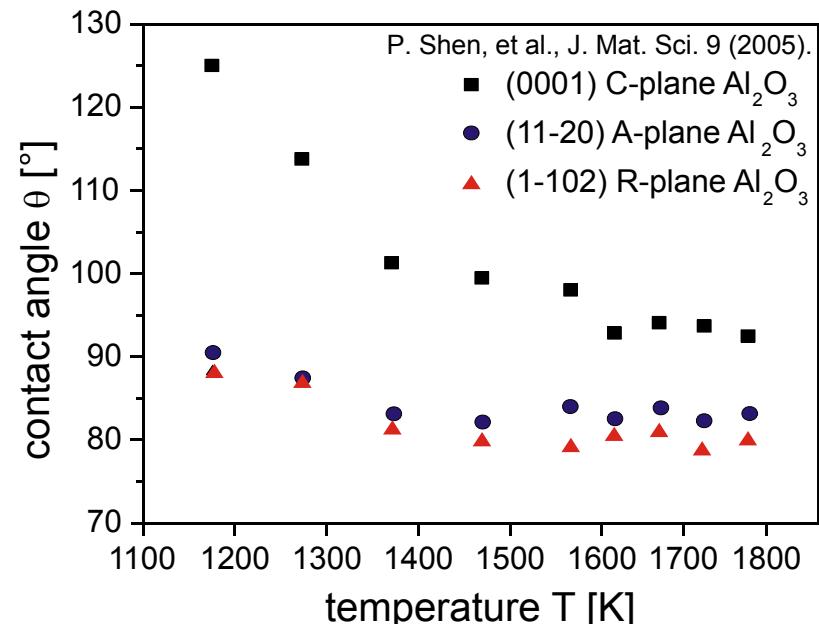


# Motivation

Isotropic wetting of Cu on  $\alpha\text{-Al}_2\text{O}_3$



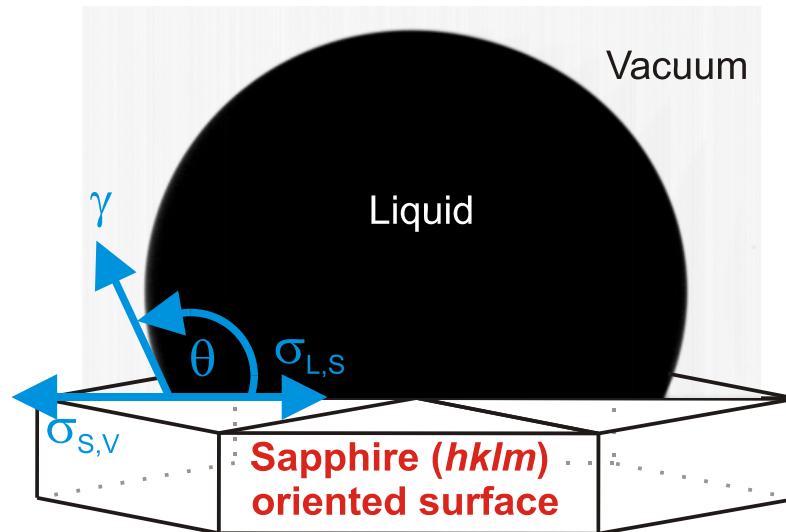
Anisotropic wetting of Al on  $\alpha\text{-Al}_2\text{O}_3$



- ↗ Wetting behaviour mostly unknown for alloys
- ↗ Al-Cu/ $\alpha\text{-Al}_2\text{O}_3$ : isotropic or anisotropic?



# Fundamentals of wetting – Work of adhesion

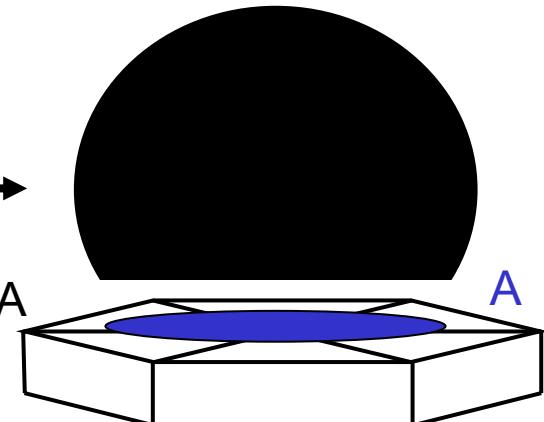


wetting:

$$E_1 = \sigma_{L,S} A$$

desorption:

$$E_2 = \sigma_{S,V} A + \gamma A$$



$$(E_2 - E_1)/A = W_{adh} = \sigma_{S,V} + \gamma - \sigma_{L,S}$$

$$\cos \theta = \frac{\sigma_{S,V} - \sigma_{L,S}}{\gamma}$$

Young equation

$$W_{adh} = \gamma(1 + \cos \theta)$$

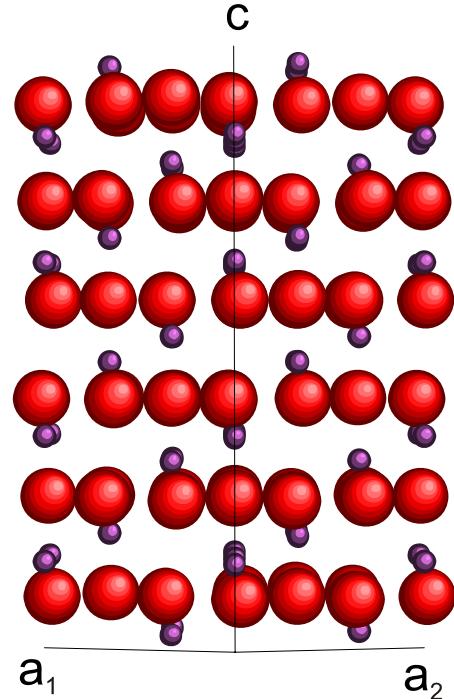
Electromagnetic levitation

Sessile drop

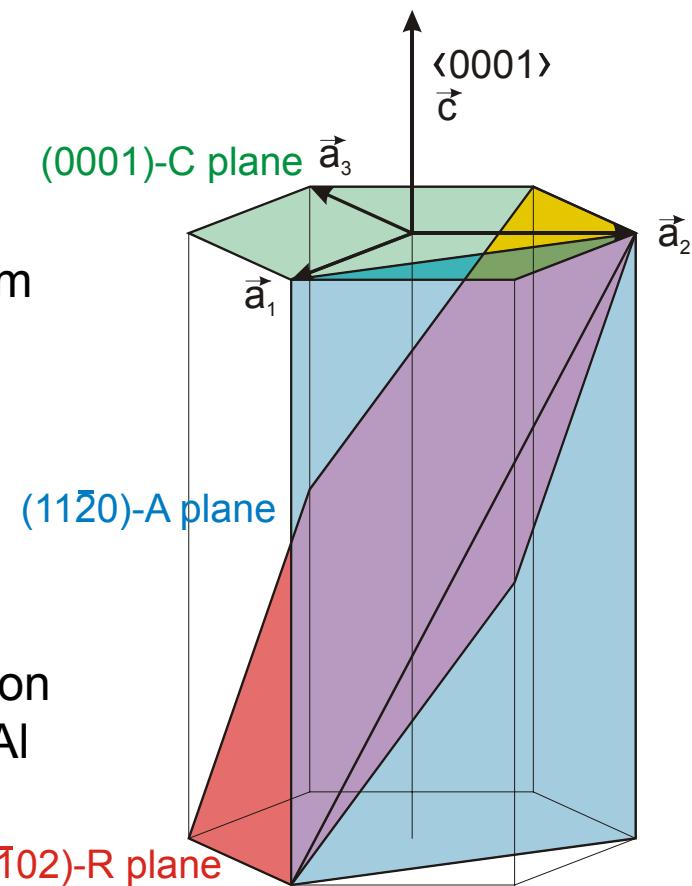


# Crystal structure of $\alpha\text{-Al}_2\text{O}_3$ (sapphire)

- ↗ hcp stacking of  $\text{O}^{2-}$
- ↗ 2/3 of octahedron sites occupied by  $\text{Al}^{3+}$



- ↗  $c=1,3 \text{ nm}, a=0,48 \text{ nm}$
- ↗ different low index crystallographic planes  
→ anisotropy
- ↗ surface reconstruction of C-plane (high T, Al vapour)

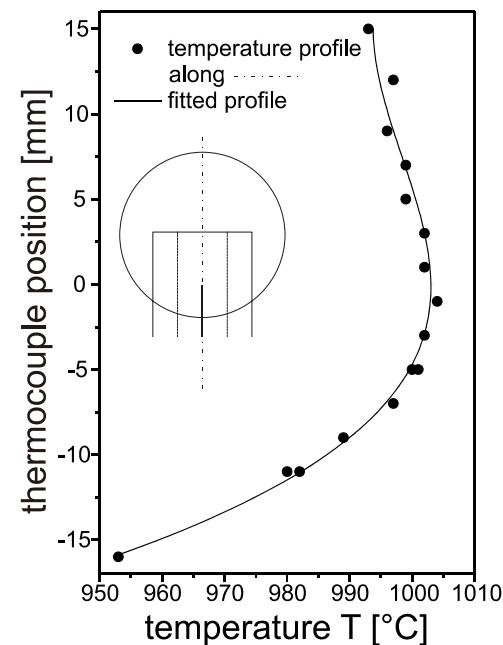
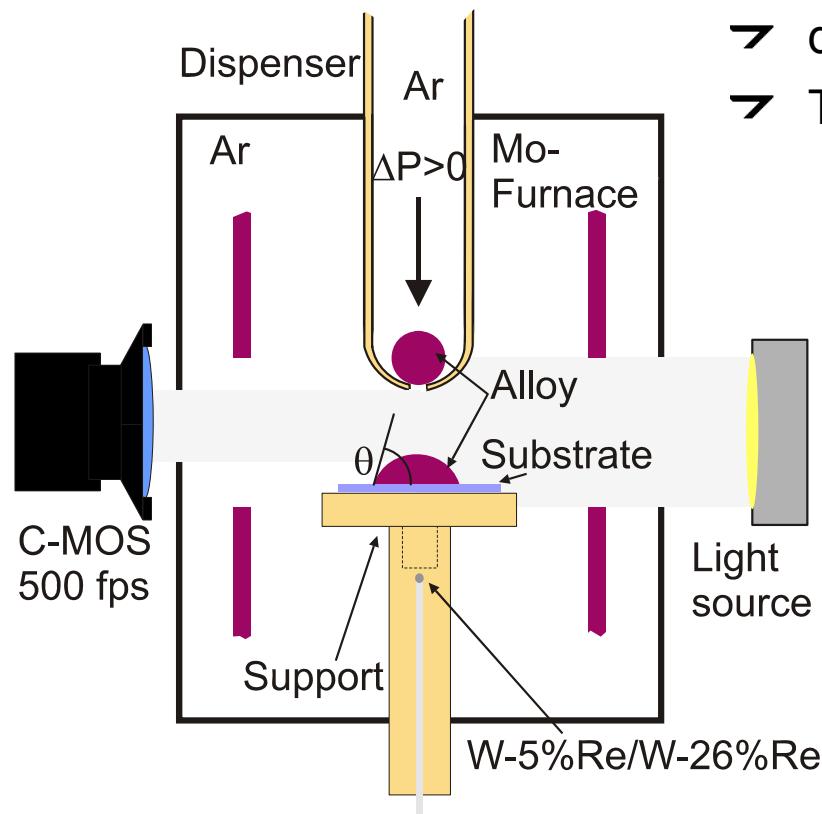




# Sessile drop apparatus

well-defined wetting conditions:

- low  $p_{O_2} (<10^{-6}$  bar)
- drop dispenser
- $T > T_L(Cu)$ ,  $dT/dx(\text{sample}) = -0,03 \text{ K/mm}$

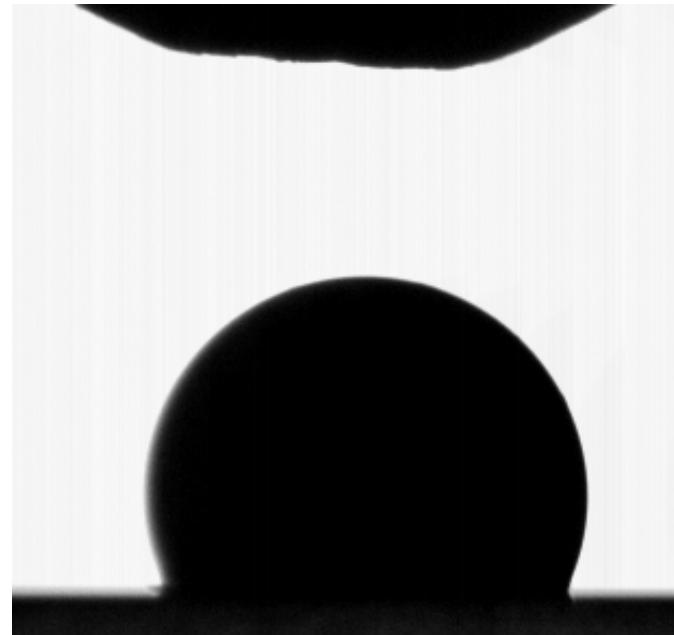
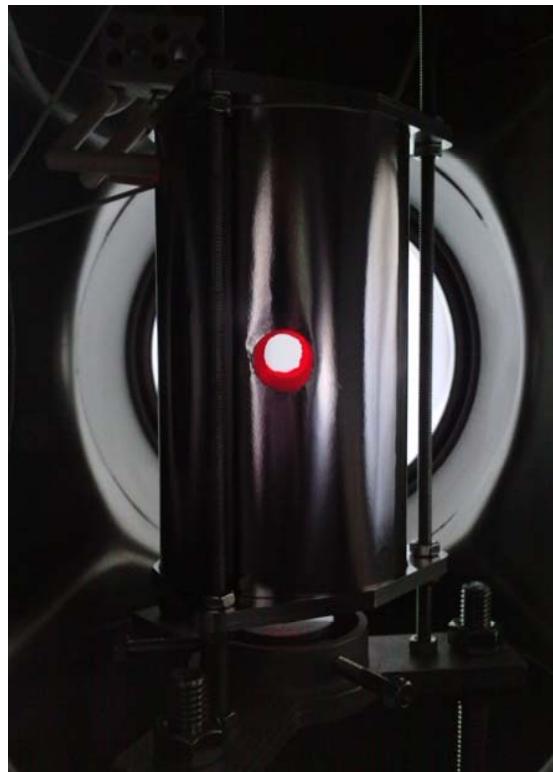




## Sessile drop apparatus

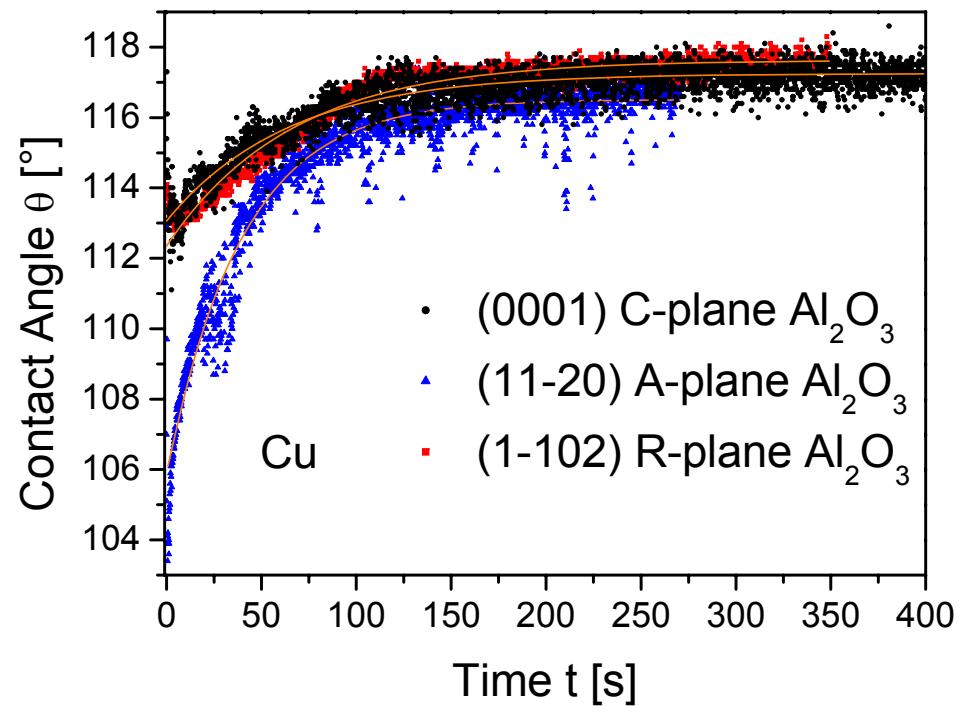
well-defined wetting conditions:

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- drop dispenser
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## Contact angle of Cu on $\alpha\text{-Al}_2\text{O}_3$ at $T = 1100^\circ\text{C}$



$$\cos \theta = \frac{\sigma_{S,V} - \sigma_{L,S}}{\gamma}$$

- Exponential increase of  $\theta$ 
$$\theta = \theta_\infty - (\theta_\infty - \theta_0) e^{-\frac{t}{\tau}}$$
 $\theta_\infty \approx 116^\circ, \theta_0 \approx 110^\circ$  (non-wetting)  
 $22\text{s} < \tau < 275\text{s}$

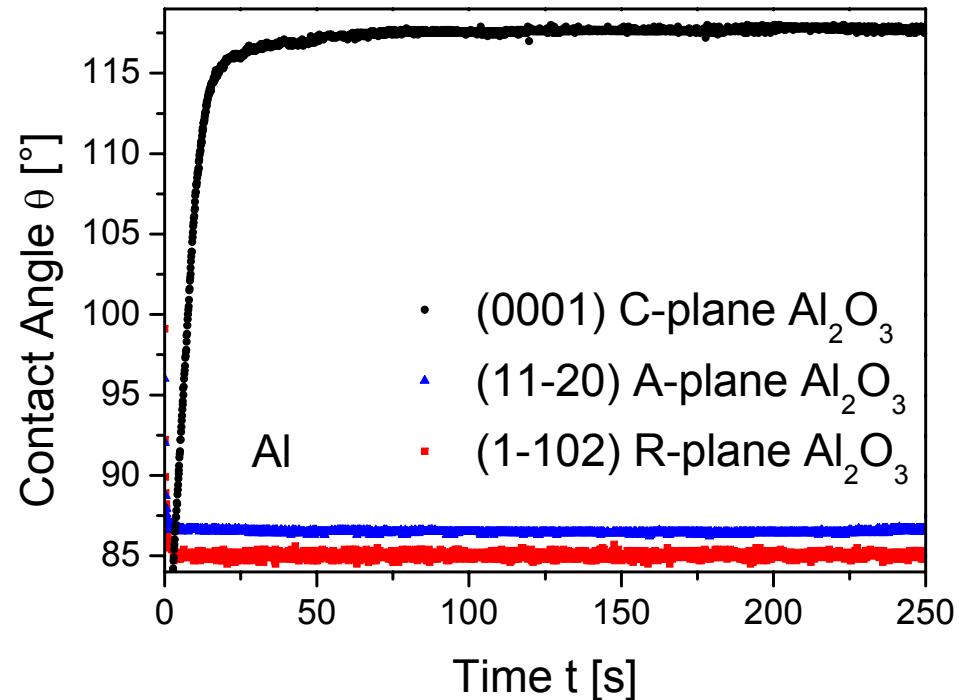
- $\theta_\infty$  in agreement with literature data<sup>1,2,3,4</sup>  
at  $10^{-12}\text{ bar} < p_{\text{O}_2} < 10^{-6}\text{ bar}$

- $\theta(t)$  due to deoxidation

- Increase of  $\sigma_{L,S}, \gamma$ 
$$\frac{d\sigma}{dt} > \frac{d\gamma}{dt}$$



## Contact angle of Al on $\alpha\text{-Al}_2\text{O}_3$ at $T = 1100^\circ\text{C}$

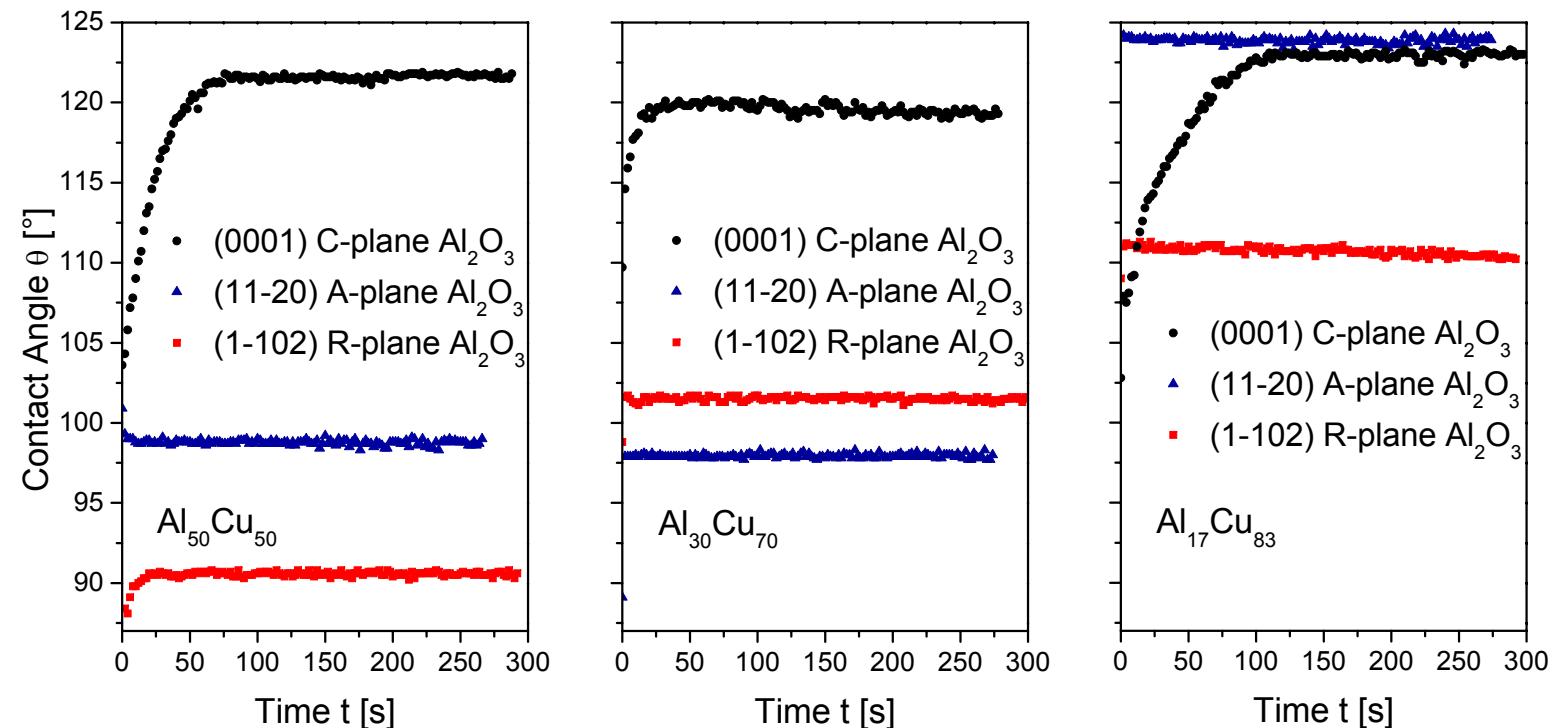


$$\cos \theta = \frac{\sigma_{S,V} - \sigma_{L,S}}{\gamma}$$

- ↗ increase of  $\theta$  only on C-plane  
 $\theta_\infty \approx 114^\circ$ ,  $\theta_0 \approx 90^\circ$ ,  $\tau \approx 10$  s
- ↗ others:  $\theta_0 \approx \theta_\infty \lesssim 90^\circ$  (wetting)
- ↗ different  $\theta(t)$ : due to surface specific processes
- ↗  $\theta > 90^\circ$ : increase due to  
$$\frac{d\sigma_{S,V}}{dt} < 0, \quad \frac{d\sigma_{S,L}}{dt} > 0$$
- ↗  $\theta_\infty$ : surface reconstruction of C-plane<sup>5</sup>  
 $\theta_0$ : unreconstructed surfaces



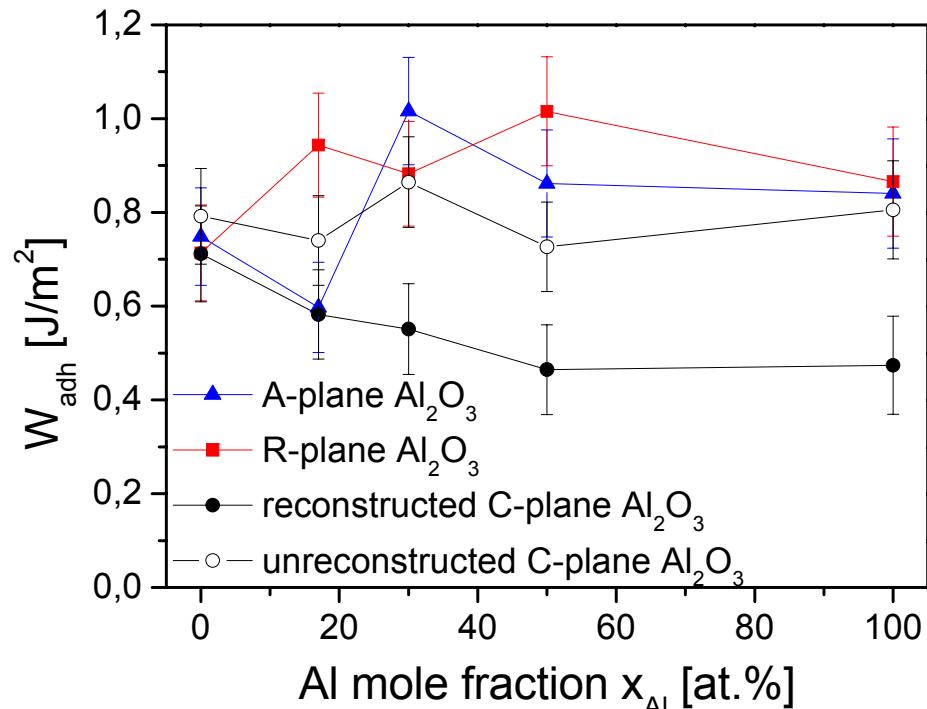
## Contact angle of Al-Cu on $\alpha\text{-Al}_2\text{O}_3$ at $T = 1100^\circ\text{C}$



- ↗ qualitative behaviour like wetting of Al on the substrates
  - ↗ No significant change in  $\theta$  for C-surfaces
  - ↗ Increase of  $\theta$  for R- and A-surfaces with  $x_{\text{Cu}}$



## Work of adhesion of Al-Cu/ $\alpha$ -Al<sub>2</sub>O<sub>3</sub> at T = 1100°C



$$W_{\text{adh}} = \gamma \cdot (1 + \cos \theta)$$

- reconstructed C-plane:  
decrease of  $W_{\text{adh}}$  with  $x_{\text{Cu}}$
- others: small increase with  $x_{\text{Al}}$
- pronounced anisotropy for  
 $x_{\text{Al}} \leq 50\%$
- thermodynamic model<sup>6</sup>  
explains behaviour for dilute  
solutions
  - adsorption of Al at each  
interface



# Atomic interactions at the Al-Cu/α-Al<sub>2</sub>O<sub>3</sub> interface

	$\varepsilon$ [kJ/mol] <sup>7</sup>
Al-Al	133
Al-Cu	217
Cu-O	269
Al-O	511

- Cu/α-Al<sub>2</sub>O<sub>3</sub>:  $\varepsilon_{\text{Cu-O}} \approx \varepsilon_{\text{Cu-Al}}$   
**wetting independent of surface termination**
- Al/α-Al<sub>2</sub>O<sub>3</sub>:  $\varepsilon_{\text{Al-O}} \approx 4\varepsilon_{\text{Al-Al}}$   
**stronger interaction with O-rich surfaces**  
reduced wetting by reconstruction  
(C-plane)
- Al-Cu/α-Al<sub>2</sub>O<sub>3</sub>: adsorption of Al  
 $x_{\text{Al}}^{\text{Interface}} > x_{\text{Al}}^{\text{Bulk}}$   
**mainly Al-Al, Al-O interactions,**  
surface termination affects wetting for  
 $x_{\text{Al}}^{\text{Bulk}} \geq 17\%$



## Summary

- ↗ no anisotropy in wetting of Cu of different  $\alpha\text{-Al}_2\text{O}_3$  surfaces (non-wetting)
- ↗ anisotropy in wetting of pure Al and Al-Cu of different  $\alpha\text{-Al}_2\text{O}_3$  surfaces:
  - ↗ Al or Al-Cu/ C-plane  $\text{Al}_2\text{O}_3$ :  $\theta_\infty \approx 120^\circ$ , decrease of  $\theta_0$  with  $x_{\text{cu}}$
  - ↗ Al or Al-Cu/ A- and R-plane  $\text{Al}_2\text{O}_3$ :  $\theta_\infty = \theta_0 = \theta_0(\text{C-plane})$  (wetting)
  - ↗ enhanced wetting of Al-rich Al-Cu alloys on A-,R- and unreconstructed C-plane  $\alpha\text{-Al}_2\text{O}_3$
- ↗ no transition isotropic-anisotropic wetting observed for low  $x_{\text{Al}}$  (17 at.%)
- ↗ behaviour of  $W_{\text{adh}}(x_{\text{Al}})$  suggests Al adsorption at surface and interface